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**UTILITY
PATENT APPLICATION
TRANSMITTAL**

(Only for new nonprovisional applications under 37 C.F.R. 1.53(b))

Attorney Docket No.	71386-6
First Inventor	Barry Reginald Hobson
Title	ELECTRIC MACHINE
Express Mail Label No.	EI 992963965US

APPLICATION ELEMENTS

See MPEP chapter 600 concerning utility patent application contents.

ADDRESS TO:

Commissioner for Patents
Box Patent Application
Washington, DC 20231

1. ☒ Fee Transmittal Form
(Submit an original, and a duplicate for fee processing)
2. ☒ Applicant claims small entity status.
See 37 CFR 1.27
3. ☒ Specification [Total Pages 29]
(preferred arrangement set forth below)
- Descriptive title of the Invention
 - Cross References to Related Applications
 - Statement Regarding Fed sponsored R & D
 - Reference to sequence listing, a table,
or a computer program listing appendix
 - Background of the Invention
 - Brief Summary of the Invention
 - Brief Description of the Drawings (if filed)
 - Detailed Description
 - Claim(s)
 - Abstract of the Disclosure
4. ☒ Drawing(s) (35 USC 113) [Total Sheets 11]
5. ☐ Oath or Declaration [Total Pages]
- a. ☐ Newly executed (original or copy)
- b. ☐ Copy from a prior application (37 CFR 1.63(d))
(for continuation/divisional with Box 17 completed)
- i. ☐ **DELETION OF INVENTOR(S)**
Signed statement attached deleting
inventor(s) named in the prior application,
see 37 CFR 1.63(d)(2) and 1.33(b).
6. ☐ Application Data Sheet. See 37 CFR 1.76

7. ☐ CD-ROM or CD-R in duplicate, large table or
Computer Program (Appendix)
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(if applicable, all necessary)
- a. ☐ Computer Readable Form (CRF)
- b. Specification Sequence Listing on:
- i. ☐ CD-ROM or CD-R (2 copies); or
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ACCOMPANYING APPLICATION PARTS

9. ☐ Assignment Papers (cover sheet & document(s))
10. ☐ 37 CFR 3.73(b) Statement ☐ Power of Attorney
(when there is an assignee)
11. ☐ English Translation Document (if applicable)
12. ☐ Information Disclosure Statement (IDS)/PTO-1449 ☐ Copies of IDS
Citations
13. ☐ Preliminary Amendment
14. ☒ Return Receipt Postcard (MPEP 503)
(Should be specifically itemized)
15. ☐ Certified Copy of Priority Document(s)
(if foreign priority is claimed)
16. ☐ Other:

17. If a **CONTINUING APPLICATION**, check appropriate box and supply the requisite information below and in a preliminary amendment, or in an Application Data Sheet under 37 CFR 1.76:

☐ Continuation ☐ Divisional ☒ Continuation-in-part (CIP) of prior application No: 09/196,274

Prior application information: Examiner Judson JonesGroup/Art Unit: 2834

For CONTINUATION or DIVISIONAL APPS only: The entire disclosure of the prior application, from which an oath or declaration is supplied under Box 5b, is considered a part of the disclosure of the accompanying continuation or divisional application and is hereby incorporated by reference. The incorporation can only be relied upon when a portion has been inadvertently omitted from the submitted parts.

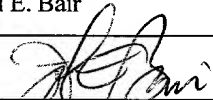
17. CORRESPONDENCE ADDRESS

☒ Customer Number or Bar Code Label **20915** or ☐ Correspondence address below

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Signature



Date

28 November 2000

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**FEE TRANSMITTAL
for FY 2001**

Patent fees are subject to annual revision

Complete if Known

Application No.	
Filing Date	
First Named Inventor	
Group Art Unit	
Examiner Name	
Attorney Docket Number	71386-6

TOTAL AMOUNT OF PAYMENT (\$) 355.00**METHOD OF PAYMENT** (check one)

1. ☒ The Commissioner is hereby authorized to charge indicated fees and credit any over payments to:

Deposit Account
Number

18-0013

Deposit Account
Name

RADER, FISHMAN & GRAUER PLLC

- ☒ Charge Any Additional
Fee Required Under
37 CFR 1.16 and 1.17
- ☐ Applicant claims small entity status. See 37 CFR 1.27

2. ☐ Payment Enclosed:

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FEE CALCULATION**1. BASIC FILING FEE**

Large Fee Code	Entity Fee (\$)	Small Fee Code	Entity Fee (\$)	Fee Description	Fee Paid
101	710	201	355	Utility filing fee	355.00
106	320	206	160	Design filing fee	
107	490	207	245	Plant filing fee	
108	710	208	355	Reissue filing fee	
114	150	214	75	Provisional filing fee	

SUBTOTAL (1) (\$) 355.00**2. EXTRA CLAIM FEES**

		Extra		below		Fee Paid
Total Claims	18	-20=	0	X		0
Independent Claims	2	- 3 =	0	X		0
Multiple Dependent						

**or number previously paid, if greater; For Reissues, see below.

Large Fee Code	Entity Fee (\$)	Small Fee Code	Entity Fee (\$)	Fee Description
103	18	203	9	Claims in excess of 20
102	80	202	40	Independent claims in excess of 3
104	270	204	135	Multiple dependent claim, if not paid
109	80	209	40	**Reissue independent claims over original patent
110	18	210	9	**Reissue claims in excess of 20 and over original patent

SUBTOTAL (2) (\$) 0**3. ADDITIONAL FEES**

Large Entity Fee Code	Small Entity Fee Code	Fee Description	Fee Paid
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105	130	205	65	Surcharge - late filing fee or oath	
127	50	227	25	Surcharge - late provisional filing fee or cover sheet.	
139	130	139	130	Non-English specification	
147	2,520	147	2,520	For filing a request for <i>ex parte</i> reexamination	
112	920*	112	920*	Requesting publication of SIR prior to Examiner action	
113	1,840*	113	1,840*	Requesting publication of SIR after Examiner action	
115	110	215	55	Extension for reply within first month	
116	390	216	195	Extension for reply within second month	
117	890	217	445	Extension for reply within third month	
118	1,300	218	695	Extension for reply within fourth month	
128	1,850	228	925	Extension for reply within fifth month	
119	310	219	155	Notice of Appeal	
120	310	220	155	Filing a brief in support of an appeal	
121	270	221	135	Request for oral hearing	
138	1,510	138	1,510	Petition to institute a public use proceeding	
140	110	240	55	Petition to revive - unavoidable	
141	1,240	241	620	Petition to revive - unintentional	
142	1,240	242	620	Utility issue fee (or reissue)	
143	440	243	220	Design issue fee	
144	600	244	300	Plant issue fee	
122	130	122	130	Petitions to the Commissioner	
123	50	123	50	Petitions related to provisional applications	
126	240	126	240	Submission of Information Disclosure Stmt	
581	40	581	40	Recording each patent assignment per property (times number of properties)	
146	710	246	355	Filing a submission after final rejection (37 CFR 1.129(a))	
149	710	249	355	For each additional invention to be examined (37 CFR 1.129(b))	
179	710	279	355	Request for Continued Examination (RCE)	
169	900	169	900	Request for expedited examination of a design application	

Other fee (specify)

*Reduced by Basic Filing Fee Paid

SUBTOTAL (3) (\$) 0**SUBMITTED BY**

Typed or Printed Name

Joel E. Bair

Complete (if applicable)

Reg. No. 33,356

Signature

Date

28 Nov 00

Deposit Account User ID

18-0013

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ELECTRIC MACHINE

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application is a continuation-in-part application of U.S. Patent Application No. 09/196,274, filed on November 19, 1998 which claims the benefit of Australian
5 Provisional Application filed on November 13, 1998.

BACKGROUND OF THE INVENTION

Field of the Invention

[0002] The applicant is knowledgeable of the design and operation of pulverizing mills used to grind mineral samples into a fine powder. The pulverizing mill together with
10 many other types of machines require an orbital or vibratory motion in order to work. These machines include for example screens for screening particles, cone crushers for crushing rocks, and shakers and stirrers for shaking and stirring laboratory solutions, biological/medical products and specifications, and the like.

[0003] The invention relates to an electric machine operable as a motor to provide
15 motion required to drive a pulverizing mill but which can alternatively be operated as a generator to provide electricity or an electrical load.

Description of the Related Art

[0004] Traditionally, the orbital or vibratory motion required on such machines is imparted to an object by attaching the object: to a spring mounted platform to which is
20 coupled an eccentrically weighted shaft driven by a motor: or, via bearings to an eccentric shaft driven by a motor. A mechanical coupling such as a gear box, belt, or universal joint is used to couple the output of the motor to the shaft.

[0005] However, the very motion that these machines are designed to produce also leads to their inevitable and frequent failure. Specifically, the required orbital or vibratory motion leads to fatigue failure in various components of the machines including mechanical couplings, transmissions, bearings, framework and mounts. The cost of repairing such failures is very high. In addition to the cost of repairing the broken component(s) substantial losses can be incurred due to down time in a larger process in which the failed machine performs one or more steps. A further limitation of such machines is that they produce fixed orbits or motions with no means of dynamic control (i.e. no means of varying orbit path while machine is running).

10 [0006] The present invention has evolved from the perceived need to be able to generate orbital or vibratory motion without the limitations and deficiencies of the above described prior art.

[0007] It is also well known in the art that an electric machine can operate as a motor when driven by electricity to provide a mechanical output such as a rotation of a shaft and, can operate as an electricity generator or electrical load when a mechanical input is provided such as a rotation of a shaft by crank, water wheel, or similar means.

SUMMARY OF THE INVENTION

[0008] According to the present invention there is provided an electric machine including:

20 a magnetic field means for producing a magnetic field having lines of flux extending in a first direction;

a support capable of at least two-dimensional motion in a plane relative to the magnetic field means and provided with a minimum of two electrically conductive paths, each path having a segment that extends through the magnetic field in a second direction

so that interaction of an electric current flowing through a particular segment and the magnetic field produces a thrust force acting on the support via that segment;

a first one of said segments located relative to a second one of said segments so that their respective thrust forces do not lie on the same axis;

5 wherein the direction and magnitude of the respective thrust forces and thus the motion of the support relative to the magnetic field means can be controlled by varying the magnitude and/or phase relationship of electric currents flowing through the segments.

[0009] Preferably, the support is made of an electrically conductive material and is
10 provided with a plurality of apertures disposed inboard of an outer peripheral edge of the support wherein the electrically conductive paths are constituted by the portions of the support that extend about the apertures.

[0010] Preferably, the support is in the form of a wheel having a central hub, spokes
extending radially outwardly from the hub and an outer rim joining the spokes, wherein
15 each aperture is defined by the space formed between adjacent spokes and sectors of the hub and rim between which adjacent spokes extend, and each conductive path comprises a pair of adjacent spokes and the sectors of the hub and rim between which the pair of adjacent spokes extend so that adjacent conductive paths share a common spoke.

[0011] Preferably, the electric machine further includes induction means for inducing an
20 electric current to flow through the electrically conductive paths.

[0012] Preferably, induction means is supported separately from the support.

[0013] Preferably, the induction means comprises a plurality of transformers each having a primary coil and a core about which the primary coil winds, and wherein the core of

each transformer interlinks with adjacent apertures so that an electric current flow in the primary coil of a transformer can induce an electric current to flow the electrically conductive paths about the corresponding adjacent apertures.

[0014] Preferably, in an alternate embodiment the induction means includes:

- 5 a transformer having a core formed into a closed loop and provided with a plurality of windows through which respective spokes of the support pass, each windows bound by opposed branches of the core that extend in the same plane as the support and opposed pairs of legs of the core that extend in a plane perpendicular to the support; and
- 10 a plurality of primary coils, a primary coil wound about at least one of the branches of the core of each window;

- whereby in use, when an alternating current is caused to flow through the primary coils lines of magnetic flux are created that circulate about the windows in the core, the majority of the flux being shared in legs of the core between adjacent windows, and wherein said lines of magnetic flux circulating about a particular window induce a
- 15 current to flow through the spoke passing through that window and the conductive paths containing that spoke.

[0015] Preferably, the segments of the conductive paths are evenly spaced by an angle 0° where 0° equals $360^\circ/\text{number of segments}$, and the currents flowing through the segments have a sequential phase difference of 0° to achieve circular orbital motion.

- 20 **[0016]** Preferably, the magnetic field producing means is a magnet provided with an air gap through which lines of magnetic flux flow and in which the segments are disposed.

[0017] Preferably, the magnet is shaped as a closed loop magnet and the air gap is formed as a closed loop.

[0018] Preferably, the magnet may be a permanent magnet or an electro-magnet.

[0019] Preferably, the magnet is in the form of a Cockcroft ring.

[0020] In the above, the machine is operated as motor to provide a mechanical output, namely the motion of the support. Additionally however, according to the invention, the

5 machine, having in general the same elements disclosed herein for the motor operation, can operate as an electricity generator or an electrical load with the addition of a mechanical input coupled to the support that will impart motion to the support in a plane relative to the magnetic field such that an electric current will be induced in the conductive paths. When operated as an electricity generator or load the machine can be
10 further simplified because the cancellation of the thrust forces, which will provide no net movement in the support in the motor operation, is not an issue when the machine is operated as a generator. The electrical equivalent to this is a generation of two currents of identical wave form but 180° out of phase with each other. But, unlike thrust forces, these currents can be individually tapped from a generator rather than combined.

15 [0021] Thus, the present invention further provides an electric machine including at least:
a magnetic field means for producing a magnetic field having lines of flux extending in a first direction; and

a support mounted for motion in at least one dimension in a plane relative to the magnetic field means and provided with at least one electrically conductive path having a
20 segment that extends through said magnetic field.

[0022] Preferably said support is made of an electrically conductive material and is provided with a plurality of apertures disposed in board of an outer peripheral edge of

said_support, wherein said at least one electrically conductive paths are constituted by portions of said support that extends about said apertures.

[0023] Preferably the support is in the form of a wheel having a central hub, spokes extending radially outward from said hub, and an outer rim joining said spokes, wherein
5 each aperture is defined by a space formed between adjacent spokes and sectors of the hub and rim between each adjacent spokes and each electrically conductive path comprises a pair of adjacent spokes and the sectors of the hub and the rim between which pair of adjacent spokes extend.

[0024] Preferably the machine further includes induction means associated with said
10 electrically conductive paths wherein electric currents flowing through said electrically conductive paths induce the current to flow through said induction means.

[0025] Preferably said induction means is supported separately from said support.

[0026] Preferably said induction means comprises a plurality of wound cores, each wound core having a core body made from a magnetically permeable material which
15 interlinks adjacent apertures and an electric coil wound about said core, each coil provided with a lead that carries an induced current generated by virtue of current flow through said electrically conductive paths extending about corresponding adjacent apertures.

[0027] In an alternate configuration said induction means includes: a core formed into a
20 closed loop and provided with a plurality of windows through which respective spokes of said support pass, each window bound by opposed branches of said core that extend in the same plane as the support and opposed legs of the core that extend in a plane

perpendicular to said support; and, a plurality of electrically conductive coils, at least one coil wound about at least one of the branches or legs of the core of each window.

[0028] Preferably the machine further includes coupling means for mechanically coupling said support to a mechanical input that moves said support in at least one
5 dimension in a plane.

[0029] Preferably the one-dimensional motion induces an electric current in the conductive paths.

[0030] Alternatively the machine further includes coupling means for mechanically coupling said support to a mechanical input that moves said support in at least two
10 dimensions in a plane.

[0031] Preferably said at least two-dimensional motion induces an electric current in said conductive paths.

[0032] In an alternate configuration the machine includes coupling means for mechanically coupling said support to a mechanical input that moves said support with a
15 non-rotary planar motion.

[0033] The present invention further provides an electric machine including at least:

a magnetic field means for producing a magnetic field having lines of flux extending in a first direction;

a support capable of at least two-dimensional motion in a plane relative to the
20 magnetic field means and provided with a minimum of two electrical conductive paths, each path having a segment that extends through the magnetic field in a second direction that has a direction component extending at right angles to the first direction.

a first one of said segments disposed at a non-diametrically opposed location on the support relative to a second one of said segments.

[0034] Preferably each conductive path is provided with a lead that carries current generated from the conductive path.

5 [0035] Preferably each lead is connected to a common junction.

[0036] Preferably the common junction is connected to a cable.

[0037] Preferably the support is rigidly attached to a mechanical input that moves the support in an at least two-dimensional motion.

10 [0038] Preferably at least two-dimensional motion induces an electric current in the conductive paths.

BRIEF DESCRIPTION OF THE DRAWINGS

[0039] In the drawings:

[0040] Figure 1A is a schematic representation of the first embodiment of the electric machine;

15 [0041] Figure 1B is an enlarged view of section A-A of Figure 1A;

[0042] Figure 1C is a graphical representation of a three-phase AC voltage/current supply;

[0043] Figure 2 is a partial cut away perspective view of a second embodiment of the electric machine;

20 [0044] Figure 3 is a partial cut away perspective view of a third embodiment of the electric machine;

[0045] Figure 4 is a partial cut away perspective view of a fourth embodiment of the electric machine;

[0046] Figure 5 is a partial cut away perspective view of a fifth embodiment of the electric machine;

[0047] Figure 6 is a partial cut away perspective view of a sixth embodiment of the electric machine;

5 [0048] Figure 7 is a partial cut away perspective view of a seventh embodiment of the electric machine;

[0049] Figure 8A is a partial cut away perspective view of a eighth embodiment of the electric machine;

[0050] Figure 8B is a perspective view of a support incorporated in the embodiment
10 shown in Figure 8A;

[0051] Figure 9 is a schematic representation of the machine depicted in Figure 1A showing the invention as an electricity generator;

[0052] Figure 10 is schematic representation of a further simplified version of the machine depicted in figure 9; and

15 [0053] Figure 11 is schematic representation of a portion of the machine depicted in figure 5 showing the invention as an electricity generator.

DESCRIPTION OF THE PREFERRED EMBODIMENT

[0054] Referring to Figures 1A and 1B, a first embodiment of the machine operates as an electric motor 10; includes magnetic field means in the form of three separate magnets
20 12A - 12C (referred to in general as "magnets 12") each producing a magnetic field having lines of flux B extending in the first direction perpendicularly into tile page. A support in the form of disc 14 is provided that is capable of two-dimensional motion relative to the magnets 12 in the plane or the page. The disc 14 is provided with a

minimum of two, and in this particular case three, electrically conductive paths in the form of conductor coils C_A , C_B and C_C (referred to in general as "conductive paths"; "coils"; or "paths" C).

[0055] Throughout this specification and claims the expression "the disc (or support)

5 is provided with electrically conductive paths" is to be construed as meaning that either the disc (support) has attached, fixed or otherwise coupled to it electrical conductors forming the paths, as shown for example in Figures 1-4; or, that the disc (support) is made of an electrically conductive material and does by itself provide or constitute the electrically conductive paths as shown for example in Figures 5-8B.

10 **[0056]** Consider for the moment the conductor path or coil C_A and its corresponding magnet 12A. The path C_A as a segment 16A that extends through the magnetic field B produced by the magnet 12A in a second direction preferably, but not essentially, perpendicular to the first direction, i.e. perpendicular to the lines of flux produced by magnet 12A. If a current is caused to flow in coil C_A say in the clockwise direction then
15 the interaction of that current and magnetic field will produce a transverse thrust force TA that acts on the disc 14 via the segment 16A. The precise direction of the thrust force TA is provided by the right hand rule and thus, in this scenario will be directed in the upward direction in the plane of the page. The remaining coils or paths C_B and C_C likewise have corresponding segments 16B and 16C that extend in a direction
20 perpendicular to the lines of magnetic flux of a corresponding magnets 12B and 12C.

Therefore, if electric currents are caused to flow in paths C_B and C_C , say in the clockwise direction, then similarly thrust forces TB and TC will be produced that act on the disc 14 via the respective segments 16B and 16C and in directions as dictated by the right hand

rule. The segments 16A and 16B (and indeed in this instance also segment 16C) are located relative to each other so that their respective thrust forces TA and TB do not lie on the same axis or line. By having two thrust forces directed along different axes or lines, two-dimensional motions of the disc 14 can be achieved. Moreover, the path of motion of the disc 14 can be controlled by varying the magnitude and/or phase relationship of the electric currents flowing through the segments 16A - 16C (referred to in general as "segments 16").

[0057] In its simplest form, consider the situation where electric current is supplied to coil C_A only in the clockwise direction. Thrust force TA is produced which causes tile disc 14 to move in the direction of the thrust force. If coil C_A is now de-energized and coil C_B energized the disc 14 will move in a direction parallel to thrust force TB which is angularly offset by 120° from the direction of thrust force TA. If coil C_A is de-energized and coil C_C energized the disc 14 will move in the direction of corresponding thrust force TC which is angularly offset by a further 120° from thrust force TB. By repeating this switching process, it can be seen that the disc 14 can be caused to move in a triangular path in a plane, i.e. it can move with two-dimensional motion in a plane. A digital controller (not shown) can be used to sequentially provide DC currents to coils C_A - C_C at various switching rates and various amplitudes for control of the motion of the disc 1A.. Also, the path or motion can be modified by causing an overlap in currents supplied to the segments. For example, current can be caused to flow in both coils C_A and C_B simultaneously, perhaps also with modulated amplitudes.

[0058] In this embodiment, three separate coils C_A, C_B, and C_C are shown. However, as is clearly apparent to produce two-dimensional motion in a plane a minimum of two

coils, for example C_A and C_B , only is sufficient, provided the respective thrust forces T_A and T_B do not act along the same axis or line. Stated another way, what is required for a two-dimensional motion is that there is a minimum of two coils relatively disposed so that when their thrust forces are acting on the disc 14 they cannot produce a zero resultant thrust force on the disc (except when both the thrust forces themselves are zero).

[0059] Rather than the triangular motion described above, the disc 14 can be caused to move with a circular orbital motion by energizing the coils C_A , C_B and C_C with AC sinusoidal currents that are 120° (electrical) out of phase with each other.

[0060] It is to be appreciated that the circular orbital motion is not a rotary motion about an axis perpendicular to the disc 14, i.e. the disc 14 does not act as a rotor in the conventional sense of the word. In the present embodiment, if each of the coils C_A , C_B , and C_C were connected to different phases in the three phase sinusoidal AC current supply, of the type represented by Figure 1C, the disc 14 would move in a circular orbital motion. This arises because the total resultant force, i.e. the combination of T_A , T_B and T_C is of constant magnitude at all times. The difference in phase between the coils C_A , C_B and C_C leads to the direction of the resultant force simply rotating about the center of (lie disc 14. This is an angular linear force, not a torque. The frequency of the motion of disc 14 is synchronous with the frequency of the AC current to the coils C_A , C_B and C_C . Thus, the motion frequency of disc 14 can be varied by varying the frequency of the supply voltage/current. A non-circular orbit can be produced by providing coils C_A , C_B , and C_C with currents that are other than 120° out of phase and/or of different amplitude.

[0061] In the embodiment shown in Figures 1A and 1B, the disc 14 is made of a material that is an electrical insulator and the coils C_A , C_B and C_C are wire coils that are fixed for

example by glue or epoxy to the disc 14. The coils C_A , C_B and C_C have separate leads (not shown) that are coupled to a voltage supply (not shown). The magnets 12 have a C-shaped section as shown in Figure 1B providing an air gap 18 through which lines of flux B extend. The segments 16 of each of the coils C are located in the air gaps 18 of their corresponding magnets 12.

[0062] Figure 2 illustrates an alternate form of the motor 10_{ii} which differs from the embodiment shown in Figure 1 by replacing the separate magnets 12A, 12B and 12C with a single magnet 12 in the form of a Cockcroft ring and in which the disc 14 is provided with six conductive paths or coils $C_A - C_F$. In order to reduce weight, the disc 14 is provided with six apertures or cut-outs 20 about which respective ones of conductive paths C extend. A multi-conductor cable 22 extends from a six phase power supply (not shown) to a central point 24 on the disc 14 where respective conductor pairs fan out to the coils C. The six phase is required for the coils $C_A - C_F$ can be obtained from a conventional star or delta three phase power supply by tapping off the reverse polarities of each phase.

[0063] In the motor 10_{ii} shown in Figure 2, each conductive path or coil C has a segment 16 that is disposed in the air gap 18 of the magnet 12. As with the previous embodiment, when current is caused to flow through the segments 16, the transverse force is created due to the interaction between the current and the magnetic flux B, the transverse force is acting on the disc 14 via the respective segments 16. It will be recognized that many different pairs of segments, (e.g. 16A, 16F; 16A, 16C; 16B, 16D etc.) are relatively located to each other so that their respective thrust forces are not parallel in the plane of motion of the disc 14. Consequently, the disc 14 is again able to move in a two-

dimensional planar motion. The fact that thrust forces produced on diametrically-opposed segments are parallel does not negate the existence of other thrust forces that do not act along the same axis or line to enable the generation of the two-dimensional planar motion.

- 5 **[0064]** In order to avoid rubbing of components and reduce friction, the disc 14 may be supported on one or more resilient mounts, e.g. rubber mounts or springs so that is not in physical contact with the magnet 12.

[0065] It would be understood that if the electric machine 10_{ii} in Figure 2 is completely turned over, a conventional grinding head can be attached to the disc 14 for grinding a
10 mineral sample. The orbital motion of the disc 14 would produce the required forces to cause a puck or grinding rings within the grinding head to grind a mineral sample. However, unlike conventional pulverizing mill, the frequency of the orbital motion can be changed at will by varying the frequency of the AC supply to the coils C. Further, the actual path and/or diameter of motion can be varied from a circular orbit to any desired
15 shape by varying the phase and/or magnitude relationship between the currents in the coils C while the machine is in motion.

[0066] A further embodiment of the electric motor 10_{iii} is shown in Figure 3. In the electric motor 10_{iii} instead of each coil C being physically connected by a conductor to a current supply through multi-connector cable 22, current for each coil C is produced by
20 electromagnetic induction using transformers 26A-26E (referred to in general as "transformers 26"). Further, the conductive paths (i.e. coils C) are now multi-turn closed loops. The disc 14 includes in addition to the apertures 20, a plurality of secondary apertures 28A - 28F (hereinafter referred to as "secondary apertures 28"), one secondary

aperture 28 being located adjacent a corresponding primary aperture 20 with the apertures 20 and 28 being separated by a portion of the coils C extending about the particular primary aperture 20. Each transformer 26 has a core 30 and a primary winding 32. The primary winding 32 may be in the form of two physically separated though electrically
5 connected coils located one above and one below the plane of the disc 14. The core 30 of each transformer links with one of the coils C so that coil C acts as secondary windings. This interlinking is achieved by virtue of the core 30 looping through adjacent pairs of apertures 20 and 28. It will be appreciated that a current flowing through the primary winding 32 of a transformer 26 will induce the current to flow about the linked coil C.
10 The apertures 20 and 28, and core 30 are relatively dimensioned to ensure that the disc 14 does not impact or contact the core 30 as it moves in its two-dimensional planar motion. The transformers 26 are supported separately from the disc 14 and thus do not add any inertial effects to the motion of the disc 14. By using induction to cause currents to flow through the coils C the need to have a physical cable or connection as exemplified by
15 multiconductor cable 22 in the motor 10_{ii} is eliminated. This is seen as being particularly advantageous as cables or other connectors may break due to fatigue caused by motion of the disc 14 and also add weight and thus inertia to the disc 14.

[0067] Figure 4 illustrates a further embodiment of the electric motor 10_{iv}. This motor differs from motor 10_{iii} by forming the respective conductive paths C with a single turn
20 closed loop conductor rather than having multiturn coils as previously illustrated. Replacing a multi-turn wire coil with a single solid loop has no adverse effects. The single solid loop behaves the same as the multi-turn coil with the same total cross-sectional area, where the current in the single loop equals the current in each turn of the

coil multiplied by the number of turns, thereby giving the same resultant thrust force.

Again, as with the previous embodiments, the motion of the disc 14 can be controlled by the phase and/or magnitude relationship of electric currents flowing through the segments 16 of each conductive path, i.e. conductive loop C.

- 5 **[0068]** Figure 5 illustrates yet a further embodiment of the electric motor 10_v. This is a most remarkable embodiment as the conductive paths C are electrically connected together. In the motor 10_v, the disc 14 is now in the form of a wheel having a central hub 34, a plurality of spokes 36 extending radially outwardly from the hub 34 and an outer peripheral rim 38 joining the spokes 36. Apertures 20 similar to those of the previous
- 10 embodiments are now formed between adjacent spokes 36 and the sectors of the hub 34 and rim 38 between the adjacent spokes 36. The disc 14 is made of an electrically conductive and most preferably non-magnetic material such as aluminum. The current paths are constituted by the parts of the disc 14 surrounding or bounding an aperture 20. For example, conductive paths CA (shown in phantom) comprises the spokes 36A and
- 15 36B and the sectors of the hub 34 and 38 between those two spokes. Conductive path C_B is constituted by spokes 36B and 36C and the sectors of the hub 34 and 38 between those two spokes. The sector of the rim 38 between adjacent spokes form the segment 16 for the conductive path containing those spokes. It is apparent that adjacent conductive paths C share a common spoke, (i.e. have a common run or log). Each transformer 26 links
- 20 with adjacent apertures 20 and has, passing through its core 30 one of the spokes 36. Consider for the moment transformer 26B. The core of this transformer passes through adjacent apertures 20A and 20B with the spoke 36B extending transversely through the core 30 of transformer 26B. The current induced into spoke 36B by the transformer 26B

is divided between current paths CB and CA. Thus the transformer 26B, when energized, induces a current to flow through both paths CA and CB. In like fashion, each of the transformers 26 can induce the current to flow in respective adjacent conductive paths C.

The state of the transformers will determine the current division between adjacent

5 conductive paths. Hence, the sectors of the rim 38 between adjacent spokes 36 and the currents flowing through them act in substance the same as the segments 16 in the motors $10_i - 10_{iv}$.

[0069] Figure 6 illustrates a further embodiment of the electric motor 10_{vi} . This motor differs from electric motor 10_v by replacing the separate transformers 26 with a multi-

10 phase toroid shaped transformer dubbed a "transoid" 40. The transoid 40 can be viewed as a ring of magnetically permeable material formed with a number of windows 42 and arranged so that separate conductive spokes 36 pass through individual different windows 42. Each window 42 is bound by opposed branches 44 and 46 that extend in the plane of the disc 14 and opposed legs 48 and 50 that extend perpendicularly to and join the

15 opposed branches 44 and 46. Primary windings 32 are placed on each of the opposed branches 44 and 46 for every window 42. (Although it should be understood that primary winding can be placed anywhere within the window i.e., 44, 46, 48, 50 with one or more primary windings being utilized in various embodiments). Primary windings 32 are coupled to a six phase current supply in a manner so that the windings 32 for each

20 window 42 are coupled to a different phase. Current flowing through the primary windings 32 sets up lines of magnetic flux circulating about the Windows 42. This flux in turn induces the current to flow in the spoke 36 passing through that window 42 and the conductive path C to which that spoke 36 relates. It will be recognized that the

majority of the flux generated about adjacent windows 42 will circulate through the common adjacent leg 48.

[0070] In comparison with the electric motor 10_v shown in Figure 5, the use of the transoid 40 makes more efficient use of its core because flux is shared from one or more primary coils. That is, magnetic flux induced by currents in primary coils about adjacent windows 42 can be shared through the common leg 48. Indeed even more distant primary coils can contribute to the flux in that leg.

[0071] A further embodiment of electric motor 10_{vii} is shown in Figure 7. This embodiment differs from the motor 10_v shown in Figure 5 in the configuration of the Cockcroft ring 12. In this embodiment, the air gap 18 of the Cockcroft ring is on the outer circumferential surface of the Cockcroft ring rather than on the inside surface as shown in Figure 5. Additionally, a plurality of radially extending slots 52 are formed in the Cockcroft ring 12 through which the spokes 36 can pass. The slots 52 must be sufficiently wide to not inhibit the motion of the disc 14.

[0072] In the embodiments of the electric motor 10_{ii} – 10_{vii} there are six segments 16 through which current flows to produce respective transverse forces that act on the disc 14. However, this can be increased to any number. Conveniently however the number of segments 16 will be related to the number of different phases available from a power supply used for driving the motor 10. For example, the motor 10 can be provided with 12 segment 16 through which current can flow by use of a 12 phase supply. In this instance, therefore, transformers are used to induce currents to flow in each segments, there will be required either 12 separate transformers 26 as shown in Figures 4, 5, and 7 or alternately a twelve window transoid 40.

[0073] In the afore-described embodiments, the motion of the support 14 is a two-dimensional motion in one plane. However, motion in a second or more nonparallel planes can also be easily achieved by the addition and/or location of further segments 16 in the second or additional planes and, further means for producing magnetic fields perpendicular to the currents flowing through those additional segments. An example of this is shown in the motor 10_{viii} in Figures 8A and 8B in which the support 14 has one set of segments 16_i and a first plane (coincident with the plane of the support 14) and a second set of segments 16_{ii} that extend in a plane perpendicular to the plane of the support 14. The motor 10_{viii} as first Cockcroft 12_{ii} having an air gap 18_{ii} in which the segments 16_i reside, and a second Cockcroft ring 12_{ii} having an air gap 18_{ii} in which the second set of segments 16_{ii} reside. Thus, in this embodiment, the support 14 can move with a combined two-dimensional motion in the plane of the support 14 and an up and down motion in a second plane perpendicular to the plane of the support 14. Thus, in effect, in this embodiment, the support 14 can float in space by action of the thrust forces generated by the interaction of the current flowing through segments 16_{ii} and the magnetic field in the Cockcroft ring 12_{ii}. As is apparent from Figure 8B the support 14 need not be circular in shape but can be square (as in Figure 8B) or any other required/desired shape. For the sake of clarity the means for supplying current to the segments 16_i, 16_{ii} have not been shown. The currents may be provided by direct electrical connection to a current source as in the embodiments 10_i and 10_{ii} or via induction as in embodiments 10_{iii} to 10_{vii}.

[0074] From the above description it will be apparent that embodiments of the present invention have numerous benefits over traditional machines used for generating vibratory

or orbital motion. Clearly, as the motion of the disc 14 is non-rotational, there is no need for bearings, lip seals, gear boxes, eccentric weights or cranks. In addition, the inertial aspects of rotation, such as a time to accelerate to speed and gyroscopic effects are irrelevant. In the embodiments of the machine 10_{ii} – 10_{vii} induction is used to cause
5 current to flow in the segments 16 and thus commutators, brushes, and flexible electric cables are not required. It will also be apparent that the only moving part of the machine 10 is either the support 14 or the magnetic field means 12. When the support 14 itself that carries the electric current as shown in embodiments 10_v - 10_{vii} this 14 can be made from one piece only say by punching or by casting. In these embodiments the disc 14
10 must be made from an electrically conductive material and most preferably a non-magnetic material such as aluminum copper or stainless steel. When the machine 10 is used to generate an orbital motion from imparting to another object (for example a grinding head) there can be a direct mechanical coupling by use of bolts or screws.

[0075] The motor 10 is a force driven machine and force it delivers is essentially
15 unaltered by its movement. There is a small degree of back EMF evident, however the tests indicate that this is almost negligible, especially when compared with conventional rotating motors. As such, the motor 10 is able to deliver full force regardless of whether the disc 14 is moving or not. For this reason, current drawn by the motor 10 is relatively unaffected by the motion of the disc 14. This enables the motion of the disc 14 to be
20 resisted or even stalled with negligible increase in current draw and therefore negligible increase in heat build-up.

[0076] In the conventional mechanical orbital or vibratory machines, the orbital or vibratory motion is usually fixed with no variation possible without stopping the machine

to make suitable adjustments. With the motor 10_i the orbit diameter is proportional to the force applied, which in turn is proportional to the currents supplied. Therefore the orbit diameter can be controlled by varying the supply voltage that regulates the current in the segment 16. This results in a linear control with instant response available, independent
5 of any other variable. As previously mentioned, the orbit frequency is synchronous with the frequency of the supply voltage, so that orbit frequency can be varied by varying the supply frequency. The motor 10 also allows one to avoid undesirable harmonics. A common problem with conventional drive systems is that as the motor builds up speed it can pass through frequency bands coinciding with the actual harmonic frequencies of
10 various attached mechanisms that can then lead to uncontrolled resonance that can destroy the machine or parts thereof. The disc 14 however is able to start at any desired frequency and does not need to ramp tip front zero speed to a required speed. In this way any undesired harmonics can be avoided. Particularly, the motor 10 can be started at the required frequency with a zero voltage (and hence zero orbit diameter) and then the
15 voltage supply can be increased until the desired orbit diameter is reached.

[0077] If no control over the orbit diameter or frequency is required, the motor 10 can be connected straight to a mains supply so that the frequency will be fixed to the mains frequency. Nevertheless, full control is not difficult or costly to achieve. Existing motor controllers which utilize relatively simple electronics with low computing requirements
20 can be adapted to suit the motor 10. Because voltage supplies can be controlled electronically, the motor 10 can be computer driven. This enables preset software program for safety features to be built into the supply controller allowing its operation to be reprogrammed at any time. The addition of feedback sensors can allow various

automatic features such as collision protection. When the disc 14 is mounted on rubber supports, it can be considered as a spring-mass system. As such, it will have a harmonic or resonance frequency at which very little energy is required to maintain orbital motion at that frequency. If the machine 10 is only required to run at one frequency, the stiffness
5 of the rubber supports can be chosen such that resonance coincides with this frequency to reduce the power losses and hence improve the machines efficiency.

[0078] While the description of the preferred embodiments mainly describes the disc 14 as moving in an orbit, depending on the capabilities of the controller for the supply, i.e. the ability to vary phase relationships and amplitudes of the supply current, the disc 14
10 can produce any shaped motion within the boundaries of its maximum orbit diameter.

[0079] Embodiments of the motor 10 can be used in many different applications such as pulverizing mills as previously described, cone crushers, sieve shakers, vibrating screens, vibratory feeders, stirrers and mixers, orbital sanders, orbital cutting heads.

[0080] Further in the described embodiments the motion of the support/disc 14 relative to
15 the magnetic field means 12 is achieved by having the support/disc 14 movable and the magnetic field means 12 fixed. However this can be reversed so that the support/disc 14 is fixed or stationary and the magnetic field means 12 moves. This may be particularly useful when it is required to impart and maintain, for example a vibratory motion to a large inertial mass. Also, it is preferred that the segments 16 extend through the magnetic
20 field B at right angles to maximize the resultant thrust force. Clearly embodiments of the invention can be constructed where the segments 16 are not at right angles, though they must have some component of their direction at right angles to the field B to produce a thrust force.

[0081] Referring now to Figure 9, the invention can also operate as an electricity generator 100. In Figure 9, the mechanical input is represented schematically by the vector 102.

[0082] The mechanical input 102 is attached to the disc 14 through a conventional connection. The input 102 and the disc 14 are connected such that the movement of the disc 14 is coextensive with the plane of the disc 14. The mechanical input 102 is provided by a conventional apparatus capable of producing a two-dimensional motion, such as a triangular or circular orbital motion. Electrical leads 104A-104C connect the coils C_A - C_C to a junction 106, to which is connected a multi conductor cable 108. The movement of the input 102 will create a corresponding movement of the disc 14. Movement of the disc 14 will induce a current in the coils C_A - C_C which will be carried through the leads 104A-104C, junction 106, and cable 108.

[0083] A more basic version of the machine 100i is depicted in figure 10. The machine 100i differs from the machine 100 of Figure 9 by the provision of a single electrical path only constituted by coil C_A . It would be appreciated that the motion provided by input 102 causing movement of the disc 14 in a plane would also lead to the induction of a current in the coil C_A which is carried through lead 104A, junction 106, and cable 108.

[0084] In a further variation of the embodiment shown in figure 10 a second electrically conductive path or coil can be provided on disc 14 diametrically opposed to coil C_A . All other parameters being equal, the currents induced in coils C_A and the diametrically opposed coil would have the same wave form but be out of phase by 180° with each. If such currents were added they will produce a nil result. However, the currents from the coils can be tapped individually. This is in contrast to the situation where the machine

having diametrically opposed coils is operated as a motor in which case the thrust forces rising from currents flowing through the coils would be diametrically opposed and, if of the same magnitude, would result in no motion, and if not of same amplitude, would cause a reciprocating motion rather than a orbital motion as ordinarily required for a pulverizing mill.

[0085] Figure 11 illustrates how the machine 100ii of figures 5 and 6 can be operated as a generator by coupling of the disc 14i to a mechanical crank 110. The disc 14i differs marginally from the disc 14 depicted in figures 5 and 6 by forming the hub support as a solid web 112 to provide for coupling of the crank 110. The crank 110 is attached to a central axis 114 of the disc 14i which is offset by distance D by a crank arm 116 from a drive axis 118. The crank 110 is rigidly attached to the disc 14i so that the application of torque about the axis 118 causes an orbital motion in a plane of the support 14i.

[0086] As with the machine depicted in figures 5 and 6 individual wound cores or the “transoid” (depicted in figure 6) can be associated with the disc 14i to effectively tap off currents induced in the separate paths C_A - C_F constituted by the support 14i.

[0087] The machine when configured as a generator illustrate in figures 9-11 can be mechanically directly coupled to the motor form of the machine depicted in figures 1-8 by a mechanical linkage between the respective discs 14. Indeed such coupling has been made in order to allow measurement of the efficiency of the motor by comparing electrical power, output and output current/voltage waveform in the generator with the electrical input to the motor.

[0088] While the invention has been specifically described in connection with certain specific embodiments thereof, it is to be understood that this is by way of illustration and

not of limitation, and the scope of the appended claims should be construed as broadly as the prior art will permit.

CLAIMS

1. An electric machine including at least:
a magnetic field means for producing a magnetic field having lines of flux extending in a first direction; and
a support mounted for motion in at least one dimension in a plane relative
5 to the magnetic field means and provided with at least one electrically conductive path having a segment that extends through said magnetic field.
2. An electric machine according to claim 1, wherein said support is made of an electrically conductive material and is provided with a plurality of apertures disposed in board of an outer peripheral edge of said support, wherein said at least one electrically conductive paths are constituted by portions of said support that extend about said
5 apertures.
3. An electric machine according to claim 2, wherein the support is in the form of a wheel having a central hub, spokes extending radially outward from said hub and an outer rim joining said spokes, wherein each aperture is defined by a space formed between adjacent spokes and sectors of the hub and rim between each adjacent spokes,
5 and each electrically conductive path comprises a pair of adjacent spokes and the sectors of the hub and the rim between which the pair of adjacent spokes extend.
4. An electric machine according to claim 3, further including induction means associated with said electrically conductive paths wherein electric currents flowing through said electrically conductive paths induce the current to flow through said induction means.
5. An electric machine according to claim 4, wherein said induction means is supported separately from said support.
6. An electric machine according to claim 5, wherein said induction means comprises a plurality of wound cores, each wound core having a core body made from a magnetically permeable material which interlinks adjacent apertures and an electric coil wound about said core, each coil provided with a lead that carries an induced current
5 generated by virtue of current flow through electrically conductive paths extending about corresponding adjacent apertures.

7. An electric machine according to claim 5, wherein said induction means includes: a core formed into a closed loop and provided with a plurality of windows through which respective spokes of said support pass, each window bound by opposed branches of said core that extend in the same plane as the support and opposed legs of the core that extend in a plane perpendicular to said support; and, a plurality of electrically conductive coils, at least one coil wound about at least one of the branches or legs of the core of each window.

8. An electric machine according to claim 1, further including coupling means for mechanically coupling said support to a mechanical input that moves said support in at least one dimension in a plane.

9. An electric machine according to claim 8, wherein the one-dimensional motion induces an electric current in the conductive paths.

10. An electric machine according to claim 1, further including coupling means for mechanically coupling said support to a mechanical input that moves said support in at least two dimensions in a plane.

11. An electric machine according to claim 10, wherein said at least two-dimensional motion induces an electric current in said conductive paths.

12. An electric machine according to claim 1, further including coupling means for mechanically coupling said support to a mechanical input that moves said support with a non-rotary planar motion.

13. An electric machine including at least:
a magnetic field means for producing a magnetic field having lines of flux extending in a first direction;

a support capable of at least two-dimensional motion in a plane relative to the magnetic field means and provided with a minimum of two electrical conductive paths, each path having a segment that extends through the magnetic field in a second direction that has a direction component extending at right angles to the first direction,

a first one of said segments disposed at a non-diametrically opposed location on the support relative to a second one of said segments.

14. An electric machine according to claim 13 wherein each conductive path is provided with a lead that carries current generated from the conductive path.

15. An electric machine according to claim 14 wherein each lead is connected to a common junction.

16. An electric machine according to claim 15 wherein the common junction is connected to a cable.

17. An electric machine according to claim 13 wherein the support is rigidly attached to a mechanical input that moves the support in an at least two-dimensional motion.

18. An electric machine according to claim 17 wherein the at least two-dimensional motion induces an electric current in the conductive paths.

ELECTRIC MACHINE

ABSTRACT OF THE DISCLOSURE

[0089] An electric motor includes a Cockcroft ring for producing a magnetic field having
5 lines of flux extending in a first direction through an air gap. A disc capable of at least
two-dimensional motion in a plane relative to the Cockcroft ring provides a plurality of
conductive paths, each path having a segment that extends through the magnetic field in a
second direction so that interaction with an electric current passing through a particular
segment produces a thrust force acting on the disc via that segment. A multiphase toroid
10 shaped transformer induces electric currents to flow in the conductive paths and thus
through the corresponding segments. The direction and magnitude of the respective
thrust forces and thus the motion of the disc relative to the Cockcroft ring can be
controlled by varying the magnitude and/or phase relationship of the electric currents
flowing through the segments.

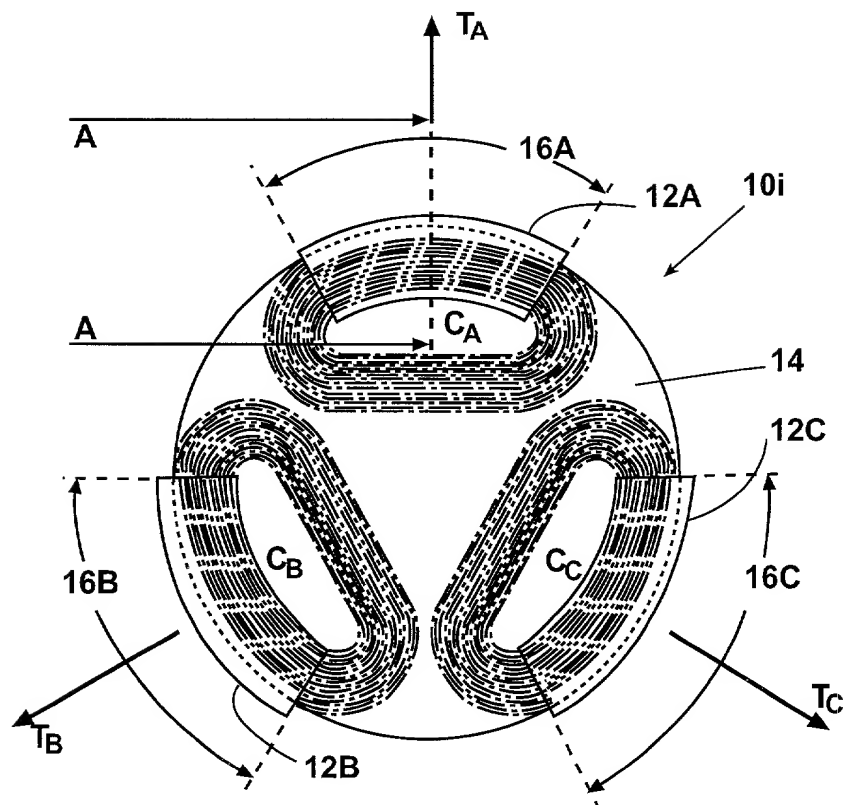


Fig. 1A

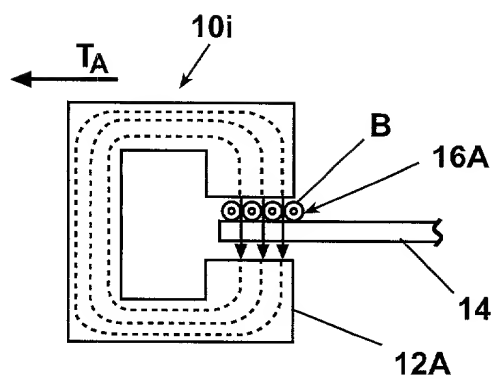


Fig. 1B

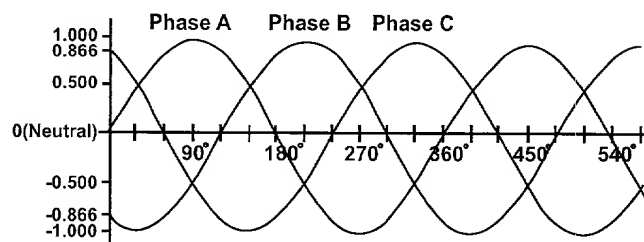


Fig. 1C

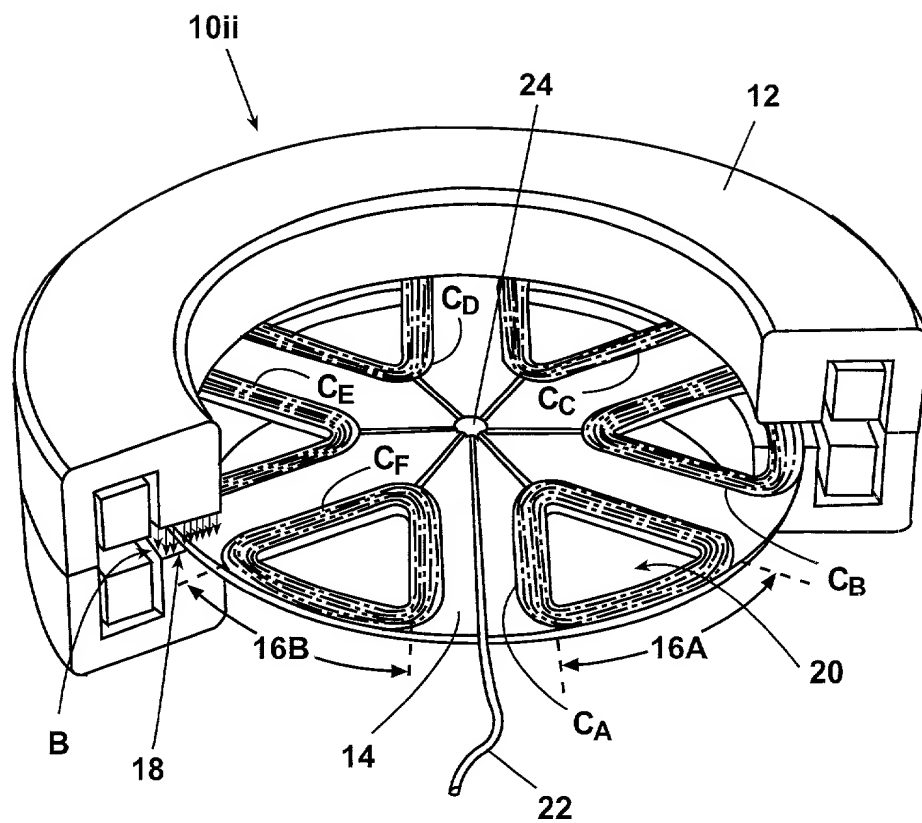


Fig. 2

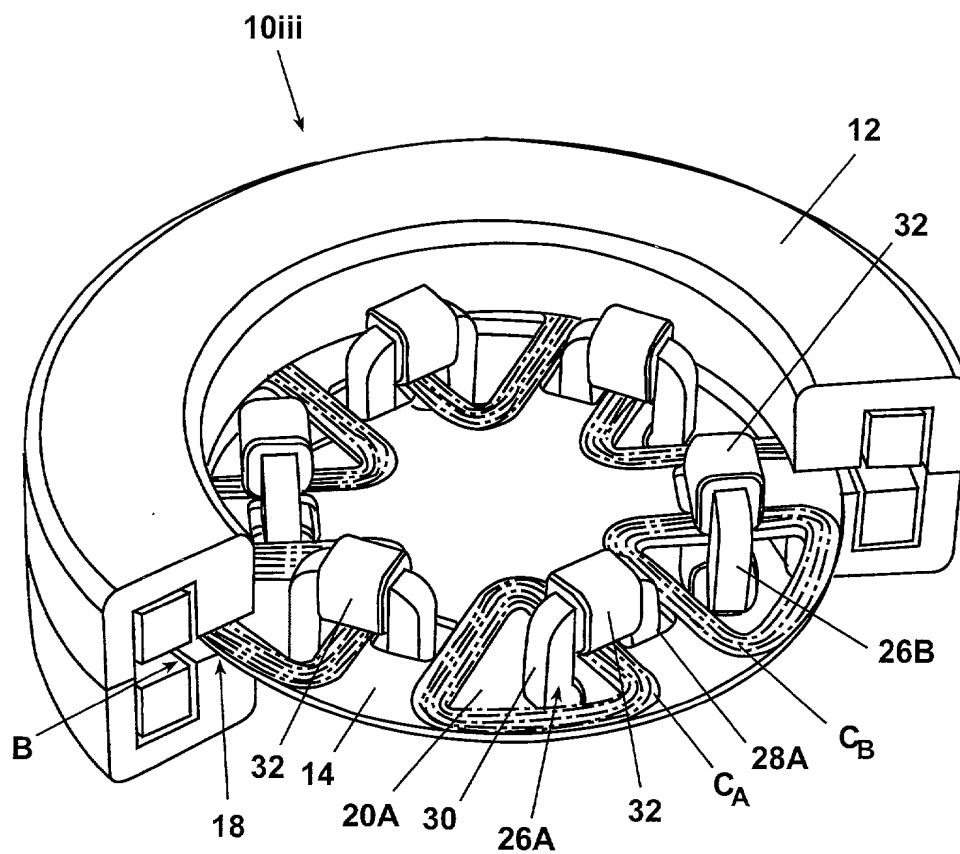


Fig. 3

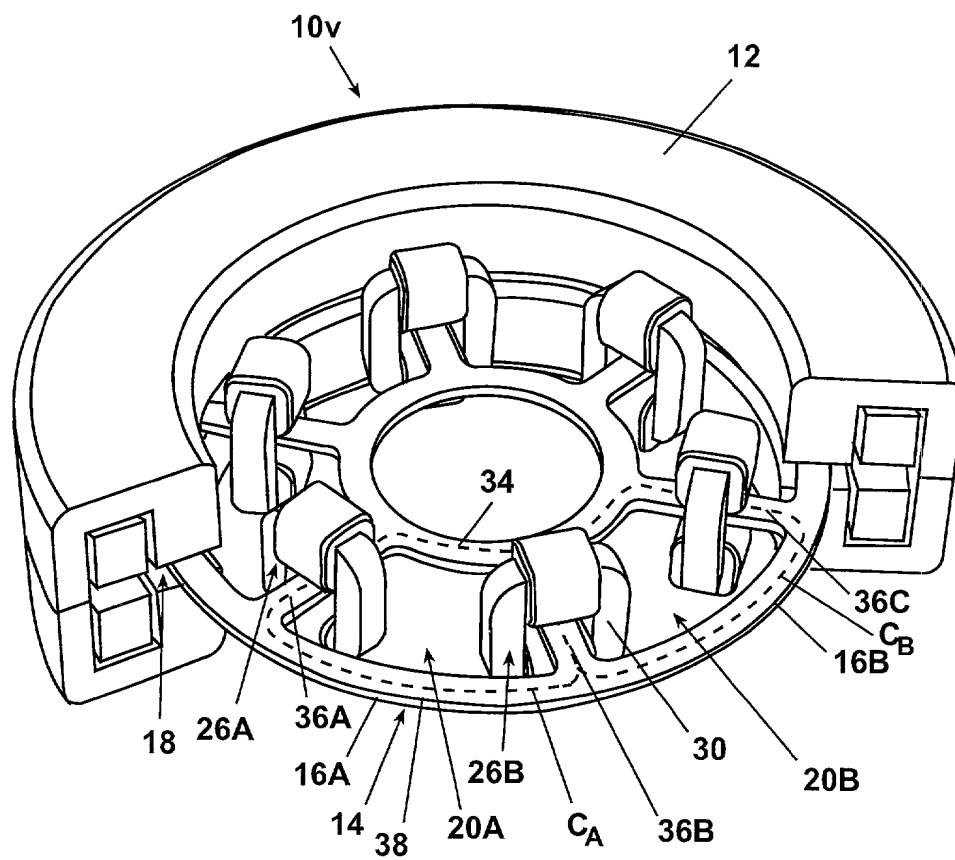


Fig. 5

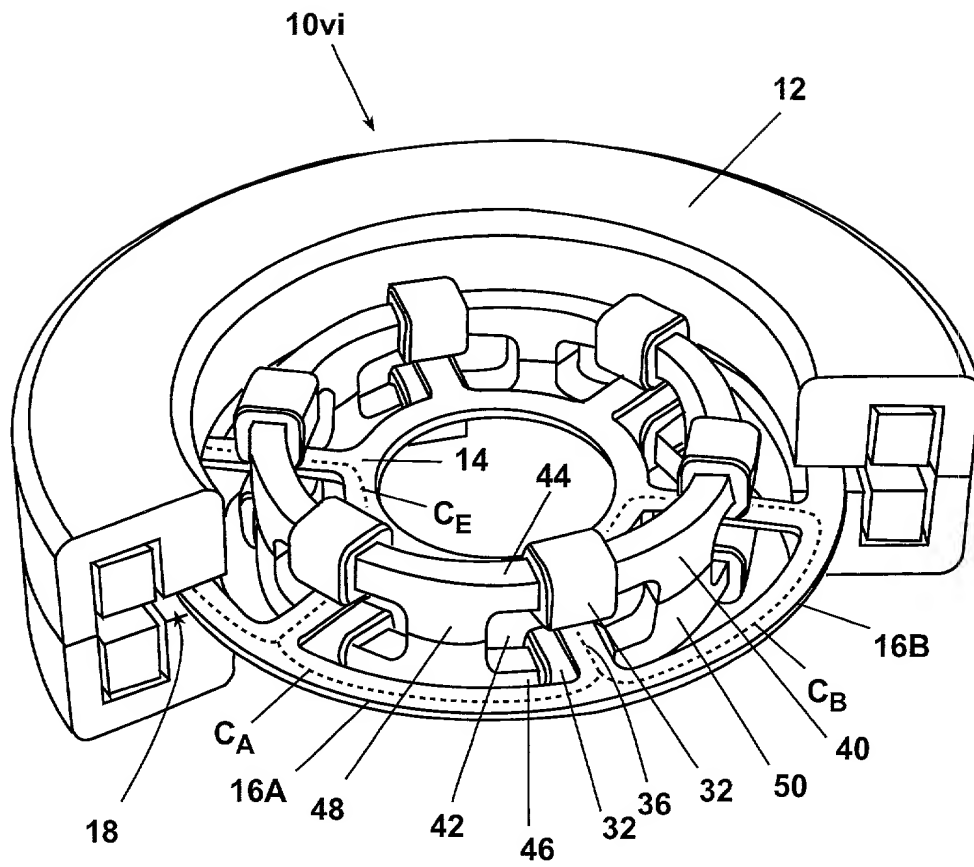


Fig. 6

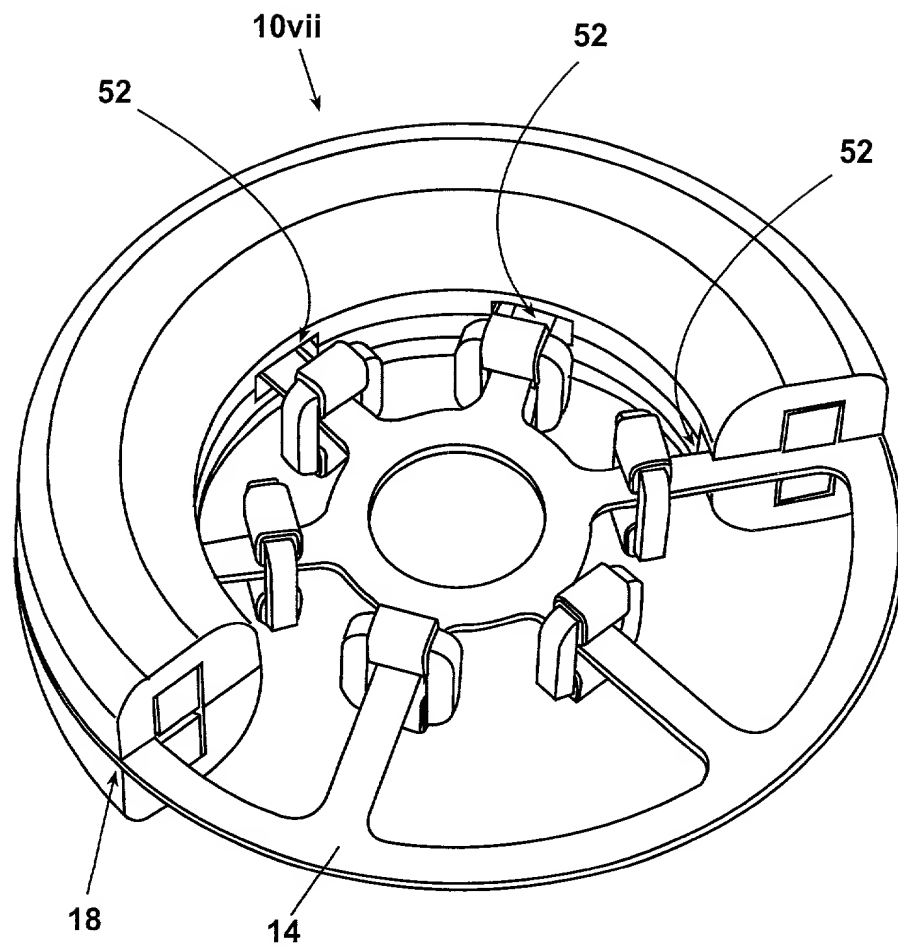


Fig. 7

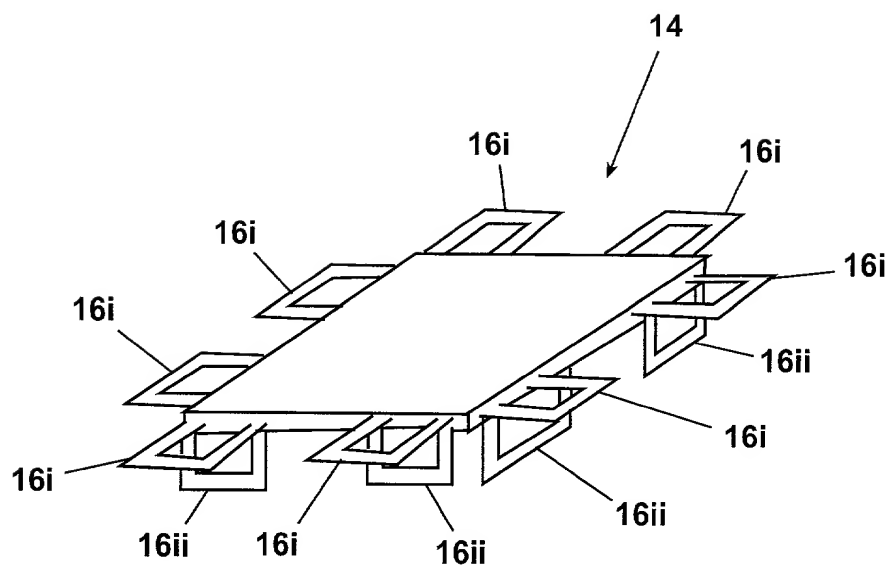


Fig. 8B

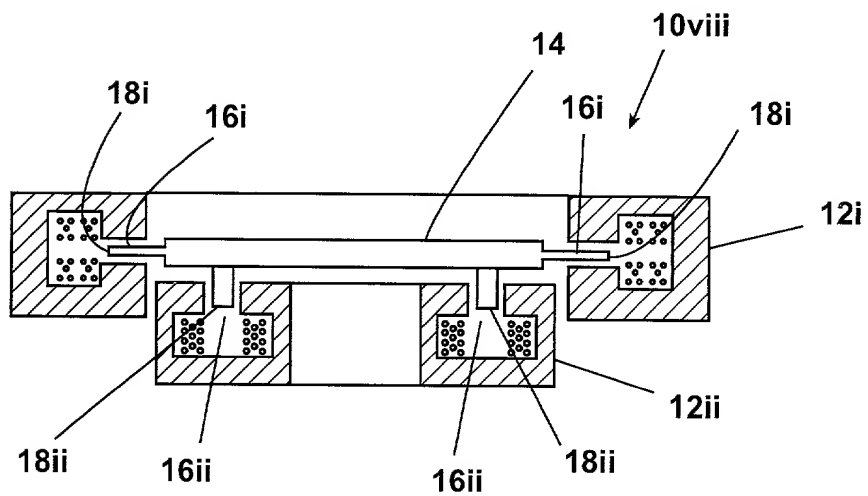


Fig. 8A

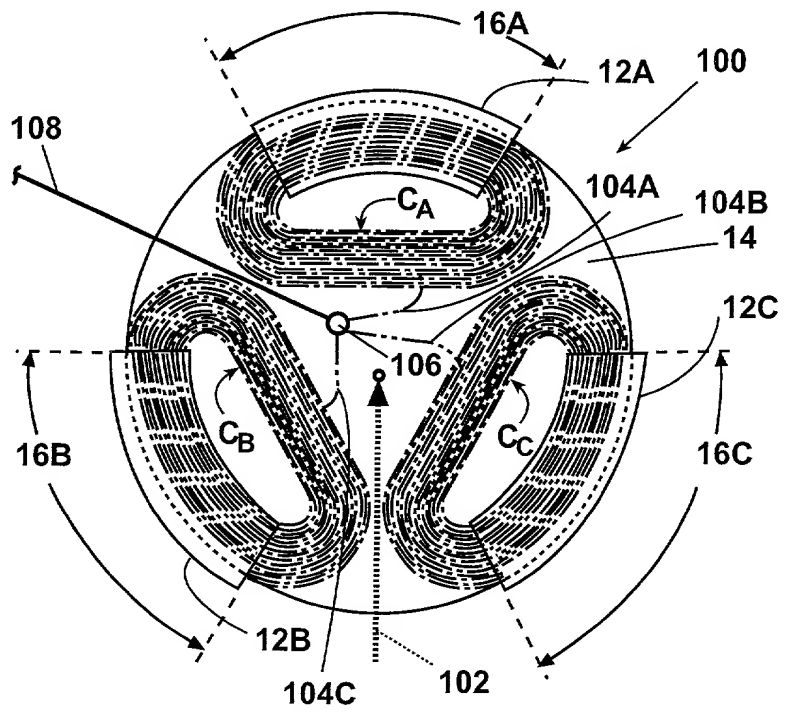


Fig. 9

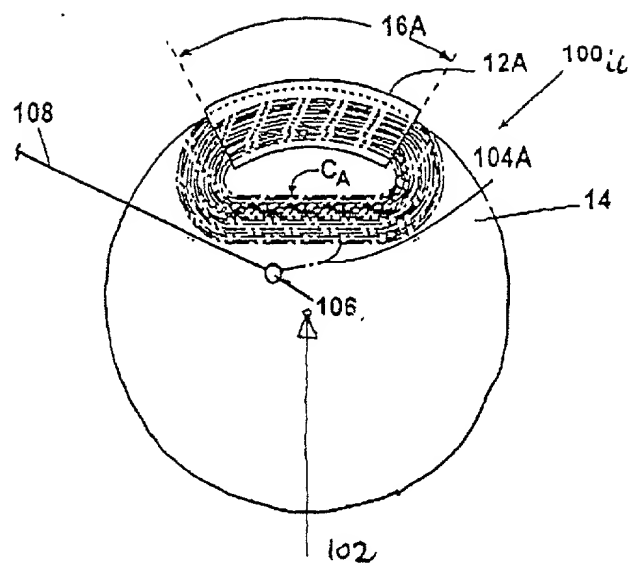


Fig 10

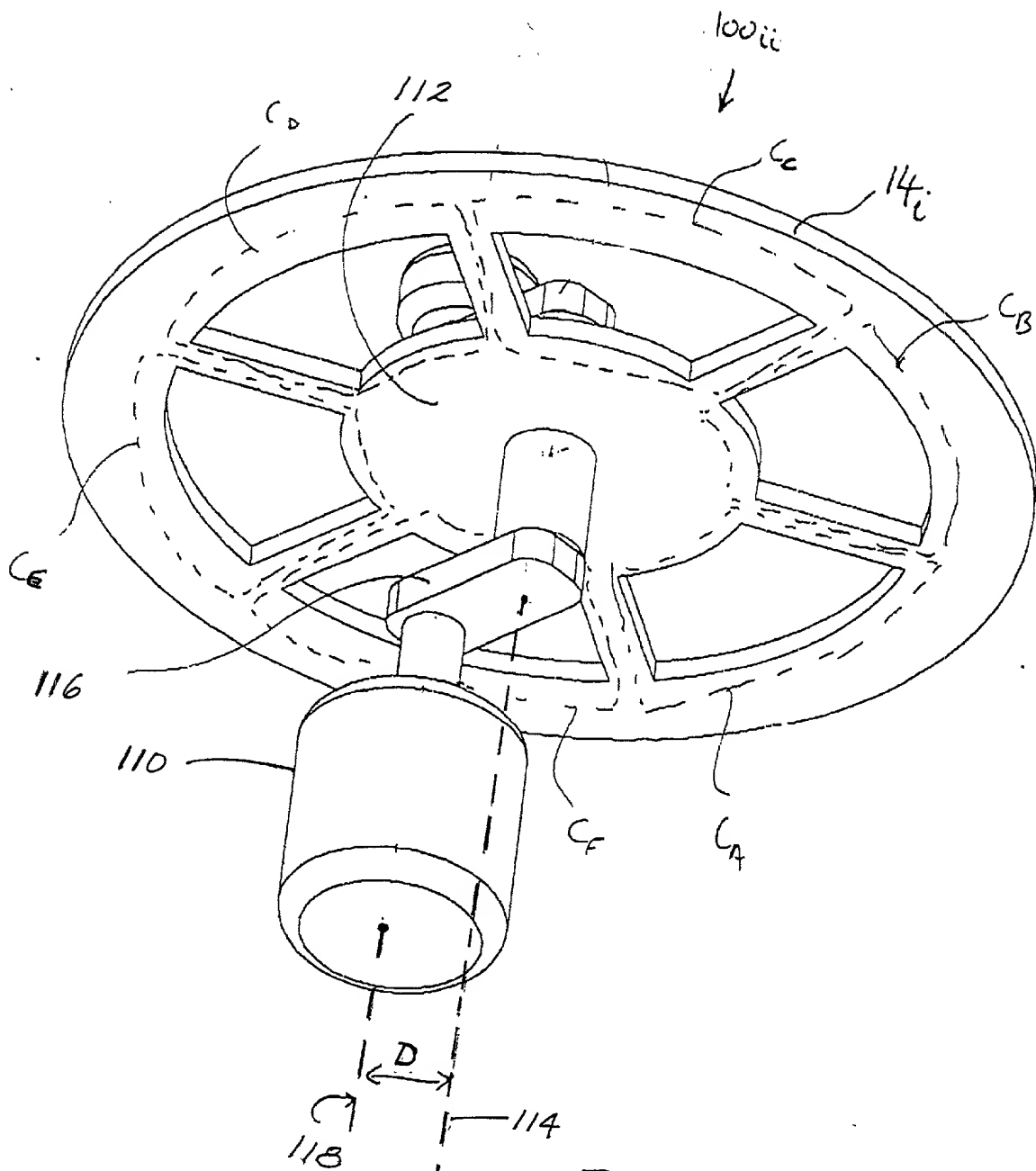


FIG 11